

Theory of Operation Document produced by Micron Eagle Hydraulics Limited

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**MICRON EAGLE HYDRAULICS LIMITED
THOERY OF OPERATION
INSTALLATION OF CURSOR WINCH ON FWD BELL SYSTEM
CSO WELLSERVICER**

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Customer: Technip UK Ltd

Project: Installation and commissioning of Cursor Winch on Fwd Bell Handling System on the CSO Wellservicer

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1.0 INTRODUCTION

Micron Eagle Hydraulics Ltd. (MEH) have been contracted to supply, install and commission the Hydraulic system for driving the Fwd Cursor Winch on the CSO Wellservicer.

1.1 Scope

The scope of this document is to provide the necessary information to Technip on the Theory of Operation of the Cursor Winch hydraulic system and interface with the existing controls.

1.2 Responsibilities

Responsibility for the issue of this document lies with the Engineer associated with the work. All requests for amendments to this document should be made to the Engineer.

1.3 Terms and Abbreviations

The following abbreviations and their meanings are used throughout this document:-

MEH	Micron Eagle Hydraulics Ltd
HPU	Hydraulic Power Unit
Client	Technip UK Ltd

1.4 Industrial Standards

P5 1991	Guidelines to Contamination Control in Hydraulic Fluid Power Systems
BS ISO 4413 1998	Hydraulic Fluid Power. General Rules Relating to Systems
BFPA Ed 8/99	British Fluid Power Association, Fluid Power Engineers Data book

2.0 General System Description

The Cursor Winch will be mounted on the Fwd Bell Handling Trolley and attached to the Cursor by means of a steel rope which will be reeved 4 times. The purpose of this winch is to provide a means of recovery in an emergency situation. In normal operation the cursor winch is required to have a constant tension mode to keep the wire rope taught while the Bell is travelling in the Moonpool.

To drive the winch in a constant tension mode additional electric motors and hydraulic pumps will need to be installed at the pump room.

To drive the winch in emergency mode the existing 35l/min supply that is already at the trolley top will be utilised.

3.0 Theory of Operation – Constant Tension

There are two electric motor / hydraulic pump sets (item 8) provided to drive the winch in constant tension mode. Only one is required for constant tension mode the second being a standby unit. At all times when the Cursor is moving one pump set must be running. These will deliver a constant flow to the raise port of the dual speed winch motor (item 2). The constant tension pressure will be set by means of an unloading relief valve (item 7) which will be located in the HPU room local to the pumps. This will need to be set during commissioning. The unloading part of the relief valve is controlled by a 24v DC solenoid valve which needs to be energised to build constant tension pressure. This would be best controlled by a timer so that the motor can start on no load and after a set time the system is 'loaded up' to the constant tension pressure. The lower port on the motor will be connected back into the 13 bar return line of the existing system at the most convenient break in point. Isolation Ball Valve BV3 (item 3) will be open for constant tension mode and closed for emergency mode. Isolation Ball Valve BV1 (item 3) will be closed for constant tension mode and open for emergency mode.

A pressure switch (item 6) has been provided in the constant tension line to allow an electrical interlock to be fitted to the system so that the bell cannot be raised or lowered unless constant tension pressure is available.

When in constant tension mode the emergency single speed winch motor (item 1) will be in a 'freewheel' mode. Isolation Ball Valve BV2 (item 5) will be open for constant tension mode.

The emergency raise / lower DCV (item 12) will remain in neutral for constant tension operation.

The Diverter valve (item 13) will be in the position shown for constant tension mode.

The brake release 24v DC solenoid valve (item 15) will be actuated from the bell winch joystick. This can be done either on the deadman switch or on the centre position switch if indeed there is one. To release the brakes the valve needs to be energised.

There is a failsafe on the brake circuit facilitated by the pilot operated DCV (item 16) which will only allow the brakes to be released when the constant tension system is healthy.



4.0 Theory of Operation – Emergency Recovery

For emergency operation the single speed motor will be used to perform the lifting of the Bell / Cursor assembly. The raise and lower function would be controlled local to the winch with the manually operated DCV (item 12). For emergency mode Isolation Ball Valve BV3 (item 3) and BV2 (item5) would be closed. Isolation Ball Valve BV1 (item 3) would be open.

Diverter Valve (item 13) must be moved to the emergency position to allow a 'bypass' around the solenoid operated brake valve (item 15). The release of the brakes will then be controlled totally by the pilot operated DCV (item 16). Diverter valve (item 18) must be moved to the emergency position to allow the brake valve (item 16) to be actuated from the Raise/Lower line shuttle valve (item 11) when in emergency mode.

5.0 Cursor / Bell Latch Cylinders

The Cursor latch cylinders will be actuated through a 24v DC solenoid operated valve which has a supply taken from the 'P' line to the emergency DCV. The supply to the Latches has a pressure reducing valve inline if needed.

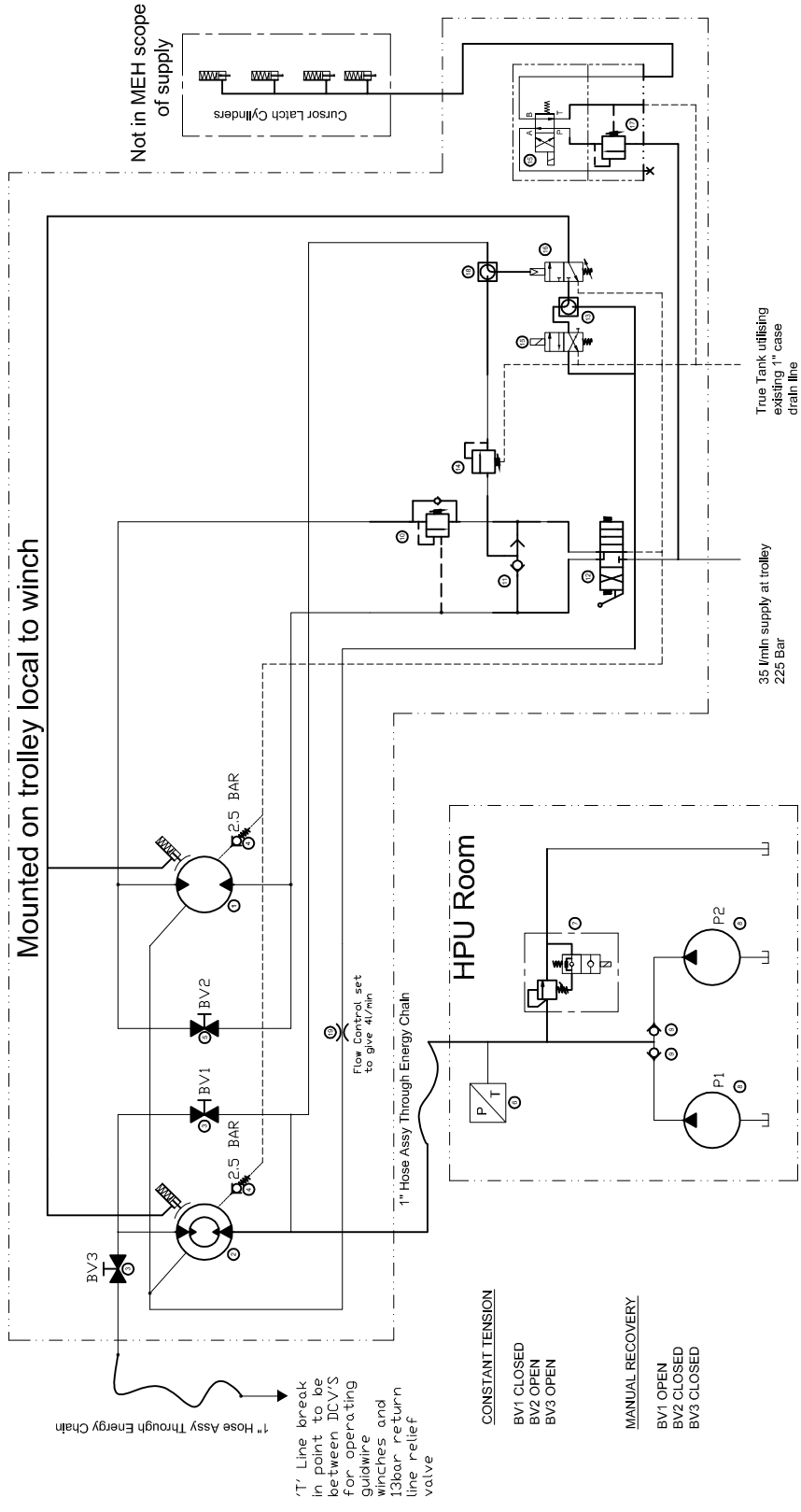
With the valve in the de-energised position no fluid will pass to the cylinders, when the valve is energised this will allow fluid to open the latches.

6.0 Console

It is our intention to mount all valves inside a control console which we will mount to the winch base on the same side of the frame as the winch base anchor point. We intend to have the Isolation Ball Valves, Diverter valve, Emergency operation DCV and pressure gauges on the console face or easily accessible from one location. We intend to include pressure gauges for system pressure, constant tension pressure and brake release pressure.

Hydraulics Circuit Schematic produced by Micron Eagle Hydraulics Limited

Mounted on trolley local to winch



CONSTANT TENSION
 BV1 CLOSED
 BV2 OPEN
 BV3 OPEN

MANUAL RECOVERY
 BV1 OPEN
 BV2 CLOSED
 BV3 CLOSED

Item Description Part No

- 1 Hagglands Single Speed Motor Supplied by Technip
- 2 Hagglands Dual Speed Motor Supplied by Technip
- 3 1" BSPP High Pressure Ball Valves BKH-1
- 4 2.5 Bar Check Valves HNRV-34-2.6B
- 5 3/4" BSPP High Pressure Ball Valves BKH-34
- 6 Rexroth Pressure Switch HED 80A 12 / 350 K14A T03
- 7 Integrated Unloading Relief Valve 7VR250P8W20-1H24S
- 8 15Kw motor c/w Marzocchi Gear Pump 3D10FG
- 9 1" BSPP check valves HNRV-1
- 10 Sun Load Holding Valve CBCG-LJN-ECV/S
- 11 3/8" BSPP Shuttle Valve SV-3 / 8-S
- 12 Walvoil DCV SD11 / 1
- 13 1/2" BSPP High Pressure 'L' Ported Valve 9105004
- 14 Integrated Pressure Reducing Valve 1PA65P3W35S-Steel
- 15 Dofluid 24V Solenoid Operated DCV DCA02-4x2-24V
- 16 Wandfluth Pilot Operated DCV AP4Z60a/63-S770
- 17 Alos Pressure Reducing Valve H3-031 / 32 / 23
- 18 1/2" BSPP High Pressure 'L' Ported Ball Valve 9105002
- 19 3/4" BSPP Flow Control NDV-G3 / 8

DO NOT SCALE
 THIS IS A CAD PRODUCED
 DRAWING AND IS NOT TO
 BE CHANGED MANUALLY
 IF IN DOUBT ASK

Revision No.	1
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Checked By	
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Micron Eagle Hydraulics	
ORIGINATOR	
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micron

CUSTOMER	Technip UK Ltd
TITLE	Fwd Cursor Winch Circuit for Wellservber including Ball Hooks
DATE	28.01.09
SCALE	N.T.S.
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Aide Memoire Document to the Project Management Handbook

Effective Management of risk is recognised throughout Technip as a key component in the successful delivery of world class projects.

The OOS Project Handbook (OOS-PMG-001) outlines the model to be followed and defines expectations for what should be achieved by Project Teams at key project stages.

This booklet acts as an aide memoire on how to achieve these expectations. It sets out the basic processes by which risks will be identified, evaluated, managed and communicated within individual projects and across the organisation.

The processes described are well tried and tested and for many this will be a reaffirmation of what they are already doing.

Nevertheless, these guidelines should drive a common language and consistency of approach which will provide a basis for learning and improvement in project delivery and the techniques used for managing project risks.

PROJECT MANAGEMENT MODEL CHECKLIST

STAGE 1 : DEFINITION OF WORKSCOPE

- ✓ Has the Project Briefing Report been completed?
- ✓ Are the Project objectives clear?
- ✓ Has Project Briefing Report been signed off by the Project Sponsor?

STAGE 2 : FEASIBILITY OF PROJECT

- ✓ Has the Project Feasibility Report been completed?
- ✓ Has the Project Schedule been checked against the corporate schedule?
- ✓ Has Project Feasibility Report been signed off by the Project Sponsor?
- ✓ Has the signed off Project Feasibility Report been placed in the Master Document Register (MDR)?
(If the Project is not feasible, move to Stage 6 and explain why it is not.)

STAGE 3 : KICK OFF

- ✓ Has the Project Presentation been completed?
- ✓ Has the attendance been recorded on the Presentation Sign Off Sheet?
- ✓ Has Presentation Sign Off Sheet been signed off by the Project Sponsor?
- ✓ Has the signed off Presentation Sign Off Sheet been placed in the MDR?

STAGE 4 : PLANNING

- ✓ Has the Project Execution Plan been completed?
- ✓ Is there a clear and detailed Project workslope?
- ✓ Has the Project Execution Plan been signed off by the Project Sponsor?
- ✓ Has the signed off Project Execution Plan been placed in the MDR?

STAGE 5 : PROJECT EXECUTION

- ✓ Is the Project following the Project Execution Plan?
- ✓ Are there any documents or drawings that need to be revised?
- ✓ Have all As Built been registered and placed in the MDR?
- ✓ Has a Project Management Report been completed?
- ✓ Is the Project complete?

STAGE 6 : PROJECT CLOSE OUT

- ✓ Are all variations, outstanding and incomplete tasks recorded?
- ✓ Are all lessons learned captured?
- ✓ Has contractor and team performance been measured?
- ✓ Has a Close Out Document Package been completed and signed off by the Project Sponsor?



Risk Assessment Report -
Installation of the Emergency Winch on the Forward Bell

DATE :	13/02/09	CLIENT :	N/A
WORKSITE :	Wellservicer	PROJECT TITLE : (if applicable)	Wellservicer emergency dry docking 2009
JOB BEING ASSESSED :	Installation of the emergency winch on the Fwd Bell	JOB SUPERVISOR (Name & Position)	
JRA REF NO: (Site or Project)		ATTENDEES (cont.)	HSE Advisor
ATTENDEES :	[REDACTED]		
REFERENCE DOCUMENTS:	Man riding winch design report OR011415DR0002 Wellservicer forward bell contingency recovery system OR011415DR0001 Bell cursor catch pivot brackets OR006491-R-001 Forward bell winch installation OR013880		
COMMENTS:			

DISTRIBUTION LIST:		JRA Reference No.:					
JOB BEING ASSESSED :		WHAT ARE THE EFFECTS:					
WHO / WHAT IS AT RISK:		WHAT ARE THE EFFECTS:					
ITEM NO.	JOB/TASK STEP	HAZARD / HAZARDOUS EVENT	CAUSES OF HAZARD OCCURRING	EXISTING CONTROLS	INITIAL RISK(IR) Sev Prob IR (eg H3 D Med)	ADDITIONAL CONTROLS/ ACTIONS ACTIONEE TIMESCALE	RESIDUAL RISK(RR) Sev Prob RR (eg H3 B Low)
1,A	Pick up drum and base from the dock bottom, using the guide wire winches to lift inboard of the vessel	Dropping of the base and drum personnel injury and damage to the equipment	Failure of attachment of rigging	Certified lifting points on the base frame, lift plan in place any additional rigging to be utilised to be certified. PTW system to be used area to be barriered off around the bottom and top of the moon pool area during lifting operations.	HDS 4B Med	Rigging plan is place (designated personnel to be allocated) all personnel to be suitably trained and experienced, good clear communications to between dock floor, bell hanger and dive control, PTW to be implemented by dive technical supervisor.	HDS 2B Low
1,B	Cross hauling into bell hanger and store in final position.	Dropping of the base and drum personnel injury and damage to the equipment, trips and falls	Failure of attachment of rigging	Certified lifting points on the base frame, lift plan in place any additional rigging to be utilised to be certified. PTW system to be used area to be barriered off around the bottom and top of the moon pool area during lifting operations.	HDS 4B Med	Once equipment is in position rigging foreman to ensure all barriers to be re-erected in bell hanger area. De rig and store items.	HDS 2B Low

2	Cursor frame to be pinned /locked off to trolley	Personnel injury Trips and falls	Dropped objects from trolley Working at height	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel only in bell hanger	HS 3 B Med	Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW.	HS 3 B low
2,A	Position bell on dry dock bottom.	Dropping the bell objects, injury to personal damage equipment.	Failure of bell wires equipment left on top of bell and surrounding area, personnel ignoring barriers.	Ensure barriers are in place around the moon pool area in the dock bottom; check the area and bell for any potential dropped objects, Designated personnel on the dock bottom in radio communication to ensure integrity of area around the bottom of the moon pool.	HDS 4B Med	Rigging plan is place (designated personnel to be allocated) all personnel to be suitably trained and experienced, good clear communications to between dock floor, bell hanger and dive control, PTW to be implemented by dive technical supervisor.	HDS 2B Low
2,B	Disconnect port and starboard bell main lift wires.	Personal injury equipment damage	Dropped objects from the bell hanger, Personnel working at height,	Ensure barriers are in place around the moon pool area in the dock bottom; check the area and bell for any potential dropped objects, Designated personnel on the dock bottom in radio communication to ensure integrity of area around the bottom of the moon pool.	HS 4B Med	Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW.	HS 3B Low
2,C	Recovery of the port and starboard bell wires to the bell hanger, and close door.	Equipment damage	Wires snagging on the bell	Wires to be monitored during the recovery operation.	D1 A Low	Good communications to be maintained during operations	D1 A Low

2.D	Lower cursor on to moon pool door	Personnel injury	Failure of cursor wire Dropped objects Working at height	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel only in bell hanger Tool box talk.	DS 4B Mid	Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW. Lift plan is place (designated personnel to be allocated) all personnel to be suitably trained and experienced, good clear communications ,tool management in place	DS 4B mid
3	Lifting of components on to trolley from bell hanger Base Drum Hydraulic motors	Dropping of any components personnel injury and damage to the equipment, trips and falls	Failure of attachment of rigging Poor rigging practice Personnel working at height,	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel only in bell hanger	DS 4B Mid	Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW. Lift plan is place (designated personnel to be allocated) all personnel to be suitably trained and experienced, good clear communications ,tool management in place	DS 4B mid
4	Assembly of winch on fwd trolley	Dropped objects personnel injury and entrapment, damage to equipment, trips and falls	Personnel working at height, and working in confined area	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel only in bell hanger Tool box talk.	HS 3 B Low	Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW.	H B 3 B Low
5	Lifting heave compensator from bell hanger to top of trolley	Dropping of any components personnel injury and damage to the equipment, trips and falls	Failure of attachment of rigging Poor rigging practice Personnel working at height,	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel only in bell hanger	DS 4B Mid	Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW. Lift plan is place (designated personnel to be allocated) all personnel to be suitably trained and experienced, good clear communications ,tool management in place	DS 4B mid
6	Lifting of hydraulic control panel from bell hanger to top of trolley	Dropping of any components personnel injury and damage to the equipment, trips and falls	Failure of attachment of rigging Poor rigging practice Personnel working at height,	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel	DS 4B Mid	Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW. Lift plan is place (designated	DS 4B mid

		falls				<p>personnel to be allocated) all personnel to be suitably trained and experienced, good clear communications ,tool management in place</p>	
7	Installation of hydraulic control panel and heave compensator. Welding and grinding operations	Personnel injury Welding sparks Fire, sparks from grinding	removal of combustible material	Ensure barriers are in place in bell hanger area potential equipment that could be affected from welding covered or removed Reference hot risk assessment	HDS 4 C Med	<p>Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW. Fire watch onsite at all time when welding and grinding designated personnel to be allocated) all personnel to be suitably trained and experienced, Earth cable to be connected close to welded area on trolley.</p>	HDS 4 B Med
8	Cursor frame work removal	Personnel injury Welding sparks Fire, sparks from grinding Working at height	removal of combustible material	Ensure barriers are in place in bell hanger area potential equipment that could be affected from welding covered or removed. Scaffolding installed inside cursor frame and external Reference hot risk assessment	HDS 4 C Med	<p>Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW. Fire watch onsite at all time when welding and grinding designated personnel to be allocated) all personnel to be suitably trained and experienced Scaffolding inspection carried out by inspector daily</p>	HDS 4 B Med
9	cursor frame installation of new sheave assembly	Personnel injury Welding sparks Fire, sparks from grinding Working at height	Failure of attachment of rigging Poor rigging practice Personnel working at height, removal of combustible material	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel only in bell hanger Scaffolding installed inside cursor frame and external Reference hot risk assessment	HDS 4 C Med	<p>Rigging plan is place (designated personnel to be allocated) all personnel to be suitably trained and experienced, PTW. Scaffolding inspection carried out by inspector daily Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW.</p>	HDS 4 B Med

10	Installation of emergency hooks on to cursor frame	Personnel injury to damage equipment.	Failure of attachment of rigging Poor rigging practice Personnel working at height,	Ensure barriers are in place in bell hanger area potential dropped objects from trolley Designated personnel only in bell hanger Scaffolding installed inside cursor frame and external	HS 3 C Med	Rigging plan is place (designated personnel to be allocated) all personnel to be suitably trained and experienced, PTW. Scaffolding inspection carried out by inspector daily Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW.	HS 3 B Low
11	Modification to bell buoyancy at hook positions	Personnel injury	Personnel working at height,	Ensure barriers are in place in bell hanger area Moon pool door close Designated personnel working on bell Scaffolding installed around bell	HS 3 C Med	Scaffolding inspection carried out by inspector daily Appropriate working at height equipment to be worn at all times, work to be controlled under the PTW. Appropriate PPE /RPE .method statement submitted	HS 3 B Low

COMMENTS:	
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REFERENCE INFORMATION FOR USE DURING THE JOB RISK ASSESSMENT
THIS INFORMATION SHOULD NOT BE CONSIDERED A COMPLETE LISTING OF ALL POTENTIAL HAZARDS AND CONTROLS.

Guidewords for Hazard Identification

Access	Coordination	Flare radiation	Other ongoing operations	Redundancy	Temperature extremes
Adequate equipment	Current	Fumes / Vapour	Overload	Release of	Traffic
Blow-on blow-off	Discharge	Environmental	Overflow	Rotation	Weather
Body positioning	Disintegration	Heave	Overpressure	Rupture	Work at height
Break / fracture	Drive	Impact	Particles	Sharp edges	
Caught between	Dropped	Injury	Pinch point	Poor visibility / lighting	
Certification	Ejection	Intakes / outlets	Portable electrical equipment	Power / Energy Isolation	
Circulation	Entanglement	Loss of power	Pollution	Recovery	
Collision	Environmental	Loss of position	Poor visibility / lighting	Slip, trip or fall	
Communication	Explosion	Noise	Power / Energy Isolation	Smoke	
Confined space	Fire	Obstructed vision	Recovery	Spillage	

Examples of Standard Control Measures Available

Task done under a Client Permit	Task done under a Technip Permit	Work equipment assessment	Mechanical isolation
Generic risk assessment in place	Lift plan in place	Certified lifting equipment	Recognised task Supervisor
Good communications (specify main parties involved)	Toolbox talk	Standard deck PPE	Good housekeeping standards

Detailed Technip procedure or work instruction	Trained, competent personnel	Technip Lifting Rules applied	Disposable oversuits
Detailed Third Party procedure	Barriers & signs erected	Certified pressure equipment	Barrier cream
Suitable environmental conditions	Tannoy announcements	COSHH assessment	Vessel DP & IMCA Common Marine Insp. Audits
Fall arrest equipment	MSDS data sheets	Electrical isolation	Correct tools

APPENDIX 1 – [TECHNIP RISK ASSESSMENT MATRIX](#)

The grid contains both alpha numeric and numeric indices (shown in brackets).

The alpha numeric indices are for categorisation of initial and residual risk.

The numeric indices are to facilitate incident categorisation for Synergi reporting purposes.

Extract from Aberdeen Hydraulics Report to the MAIB

5 Brake Failure Scenarios

Power Pack Running

1. Pressure reducing valve (14) traps pressure on to the pilot of variable pilot valve (16), thus allowing pressure through to release the brakes.
2. Pressure reducing valve (14) delays the pilot venting from variable pilot valve (16), thus causing a delay in the brakes applying.
3. Variable pilot valve (16) sticks in the operated position due to contamination, thus allowing pressure through to release the brakes.
4. Very high tank pressure in excess of 16 Barg, thus allowing the brakes to release via the "T" port of variable pilot valve (16).

Power Pack Not Running

5. Obstruction in the brake line between the brake and variable pilot valve (16), thus preventing the brake actuators from venting when the variable pilot valve (16) is in the spring offset position.
6. Obstruction in the "T" line from variable pilot valve (16), thus preventing the brake actuators from venting when the variable pilot valve (16) is in the spring offset position.

The brakes would however apply in scenarios 1,2,3 when shutting down the power pack. Power pack run down time would be a consideration of how long the brakes would remain released until the pressure in the system decays to below 16 Barg.

Dependent on the source of back pressure of scenario 4, the brakes may or may not apply when the power pack is shut down.

The brakes would not apply immediately in scenarios 5 & 6 if the power pack was shut down. The pressure may however leak away over a period of time dependent on internal leakage of variable pilot valve (16) and or the nature of the obstruction.

6 Winch Load Holding Capabilities Scenarios (Manual Recovery Only)

Dynamic braking in this circuit is achieved by counterbalance valve (10) even without the brakes applied in a correctly configured circuit with the power pack running the winch should not lower off uncontrolled. The winch however would creep due to internal leakage.

Insufficient Charge Pressure

Failure to ensure adequate charge pressure at the low pressure side of the motor to ensure the piston pressure is greater than the case pressure will have the tendency for the motor to go into “free wheel” mode once the oil which is supporting the load against the counterbalance valve (10) is exhausted. In all circuits natural leakage is experienced due to normal clearances between moving parts and to a greater extent in worn systems. Once the oil leaks away the counterbalance valve (10) becomes ineffective.

Oil leaking away from the pistons allows the motor to rotate. The pistons which are open to tank will have the tendency to be pushed in by the case pressure. When these pistons disengage from the Cam ring the motor is not capable of supporting any load.

Incorrect Counterbalance Valve Setting

The counterbalance valve comes with a factory setting of 210 Barg. Allowing for a maximum load induced pressure of 161 Barg. Counterbalance valves should be adjusted to approximately 130% of the maximum load induced pressure present to ensure the valve is fully seated.

A point to note is that with this model of counterbalance valve, **anti clockwise** rotation increases the set point of the valve.

7 Calculations

Line Pull- Cursor only

$$\text{Line Pull (Te)} = \frac{(\text{Cursor Mass(Te)} + \text{Rope Mass(Te)}) * \text{Sheave Eff.} * \text{Bearing Eff.}}{\text{No. of Falls}}$$

$$\text{Line Pull (Te)} = \frac{(4 + 1) * 1.12 * 1.05}{4}$$

$$\text{Line Pull (Te)} = \underline{1.54 \text{ Tonnes}}$$

Drum Torque

$$\text{Drum Torque (Nm)} = \text{Line Pull (Kg)} * 9.807 * \text{Working Radius (m)}$$

$$\text{Drum Torque (Nm)} = 1540 * 9.807 * 0.3563$$

$$\text{Drum Torque (Nm)} = 5381 \text{ Nm}$$

Pressure Required

$$\text{Pressure (Barg)} = \frac{\text{Drum Torque (Nm)} * 20 * \text{PI}}{\text{Motor Displacement (cc/rev)} * \text{eff}}$$

$$\text{Pressure (Barg)} = \frac{5381 * 20 * \text{PI}}{9204 * 0.95}$$

$$\text{Pressure (Barg)} = 38.6 \text{ Barg}$$

Line Pull- Cursor and Diving Bell.

$$\text{Line Pull (Te)} = \frac{(\text{Cursor (Te)} + \text{Bell (Te)} + \text{Rope (Te)}) * \text{Sheave Eff} * \text{Bearing Eff}}{\text{No. of Falls}}$$

$$\text{Line Pull (Te)} = \frac{(4 + 11 + 1) * 1.12 * 1.05}{4}$$

$$\text{Line Pull (Te)} = \underline{4.7 \text{ Tonnes}}$$

Drum Torque

$$\text{Drum Torque (Nm)} = \text{Line Pull (Kg)} * 9.807 * \text{Working Radius (m)}$$

$$\text{Drum Torque (Nm)} = 4700 * 9.807 * 0.3563$$

$$\text{Drum Torque (Nm)} = 16423 \text{ Nm}$$

Pressure Required

$$\text{Pressure (Barg)} = \frac{\text{Drum Torque (Nm)} * 20 * \text{PI}}{\text{Motor Displacement (cc/rev)} * \text{eff}}$$

$$\text{Pressure (Barg)} = \frac{16423 * 20 * \text{PI}}{9204 * 0.95}$$

$$\text{Pressure (Barg)} = 118 \text{ Barg}$$

The above calculations identify that only approximately 38.6 Barg of pressure is required to support the mass of the cursor with approx 1 Tonne of rope paid out and 118 Barg of pressure to support the mass of the cursor and bell, again with approximately 1 Tonne of rope paid out.

This would indicate that the counterbalance valve at its factory setting of 210 Barg would be capable of supporting the mass of the cursor, rope and bell.

8 Conclusions

8.1 In order for the cursor to descend unaided the following conditions would have to be met: -

- Brakes Released
- Hydraulic Integrity compromised

8.2 With reference to the section above Brake Failure Scenarios there are multiple reasons to why the brakes would have remained in the released position. This will require further investigation to pin point the root cause of failure.

8.3 The utilisation of the Hagglunds motor and the failure to adhere to the manufacturers recommendations in respect to supplying sufficient charge pressure directly impacts on the load holding capabilities of the motor when used in a lifting application.

8.4 The failure of not using the uppermost port of the Brake actuator although not in line with the manufactures recommendations, it is not felt that this would have a detrimental effect on the brake actuator operation.

8.5 The brake adjustment on both brake bands were found to be out with tolerance but at time of inspection the Cursor winch was suspended and held.

Extract from Control Panel Inspection Report carried out by SMS Consultants, University of Bath

1. Summary.

A hydraulic pilot operated directional control valve was examined in order to determine the cause of an operational malfunction that resulted in the failure of the brake on a hydraulic crane motor to lock the motor in position, thereby allowing the suspended load to fall after several minutes.

The probable cause has been attributed to the restriction of free movement of the flow control spool back to the fully closed position, caused by material deformation around the lip of the spool bore at the pilot chamber end of the valve body. This deformation appears to have been caused by high localised stresses around the bore lip, attributable to a thin ring of raised material located on the underside surface of the spool shoulder. This ring of material appears to be the result of incomplete machining of the undercut to the spool shoulder. The effects of this plastic deformation have been exacerbated by the apparent lack of concentricity of the pilot chamber recess relative to the spool bore which has resulted in an asymmetric countersink chamfer around the bore lip.

It has not yet been determined why the pressure in the brake line did not drop sufficiently through internal leakage past the spool to allow the brake to operate. Tests have shown that brake line pressure can be retained above 40 bar by a similar valve with the spool fixed in the same position as that of the malfunctioning valve for a period in excess of 18 hours. It has been stated that the brake is held off by pressures above approximately 23 bar.

The origin of the wear marks observed on the inner surface of the adjuster spring chamber has not been determined.

MAIB Flyer

FLYER TO THE SHIPPING INDUSTRY Fatality on the diving support vessel *Wellservicer*



A crew member suffered fatal injuries while carrying out modification work on the diving bell recovery system of the diving support vessel *Wellservicer*.

The modifications were part of an upgrade to enable recovery of the bell in the event of the main bell winch system failure. This involved the installation of a new winch arrangement for the bell's cursor¹.

The new winch had been operational for several days, but had not been fully commissioned. Before the accident, the new winch was used to raise the 4 tonne cursor to allow riggers to work on top of the bell. The winch system was designed such that the brake was automatically applied when the winch control was placed in the neutral position and when hydraulic power was removed.

Once the cursor was in position the brake of the new winch was applied to lock it in position. Several riggers then worked on top of the bell for a period of time.

Part of the modification required the removal of buoyancy blocks from the top of the diving bell. A rigger climbed on top of the bell to do this, but the blocks were very cumbersome and it became apparent that the cursor would have to be raised further to enable the blocks to be removed. Power was applied to the new winch and an operator went to a control position sited above the cursor and diving bell from where he began to raise the cursor. From the control position, the operator was unable to see the top of the diving bell and he was directed by a rigger using hand signals from a visible part of the deck below. Once the cursor was at a suitable height, lifting was stopped, power to the winch was switched off and work on top of the bell set to continue. A few seconds later the winch rendered and the cursor fell, trapping the rigger between the diving bell and the cursor.

Despite his colleagues' best efforts and rapid evacuation to hospital, the rigger died from his injuries.

The cause of the winch failure was attributed to a faulty pilot valve in the cursor's winch control system, which prevented the winch brakes from applying once hydraulic power was removed.

¹ Cursor: An arrangement in the shape of an inverted bowl, which guides the diving bell into the ship from below, whereupon the two mate, enabling the diving bell to become integral with the ship and her movements.

Safety Issues

- The installation team failed to apply the most basic of safety principles while working under the suspended load. Regardless of whether the winch had been commissioned and declared fully functional, the cursor should have been supported by additional means, before anyone went underneath it.
- It is extremely inadvisable to place any confidence in the safe operation of machinery that has not been fully commissioned and which therefore has not been properly tested.
- The design of the hydraulic circuit for the new cursor winch meant that the two brakes fitted to the winch did not operate independently, as they were required to do, since a single, defective, pilot valve was common to both brake circuits.
- At the time of the accident, the design of the winch's hydraulic system had not been approved by the vessel's operators or the classification society tasked with approving the whole system. Had such approval been sought for the hydraulic system it is highly probable that the anomaly in the brake circuit design, as highlighted above, would have been identified. Formal approval of systems and their component elements is an essential safety barrier which should never be circumvented before equipment is used.
- *Wellservicer's* operators had numerous management procedures and safety tools in place to ensure safe working. These were either not applied or were applied ineffectively, to the extent that no-one recognised the risk posed by the suspended cursor. Safety management systems and procedures are useless if their purpose is not understood and applied with diligence by all stakeholders.
- Lines of responsibility between the vessel and shore-based staff became confused. As a result, overall management of the modification project lacked direction and control. Responsibilities should be clearly defined, and understood; it is better to ask too many questions than to carry on with a potentially hazardous task in blind faith that other people are doing what is expected of them.

This accident was subject to MAIB investigation, the report of which can be found on the MAIB's website at:

www.maib.gov.uk

A copy of the flyer and / or the report will be sent, on request, free of charge.

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